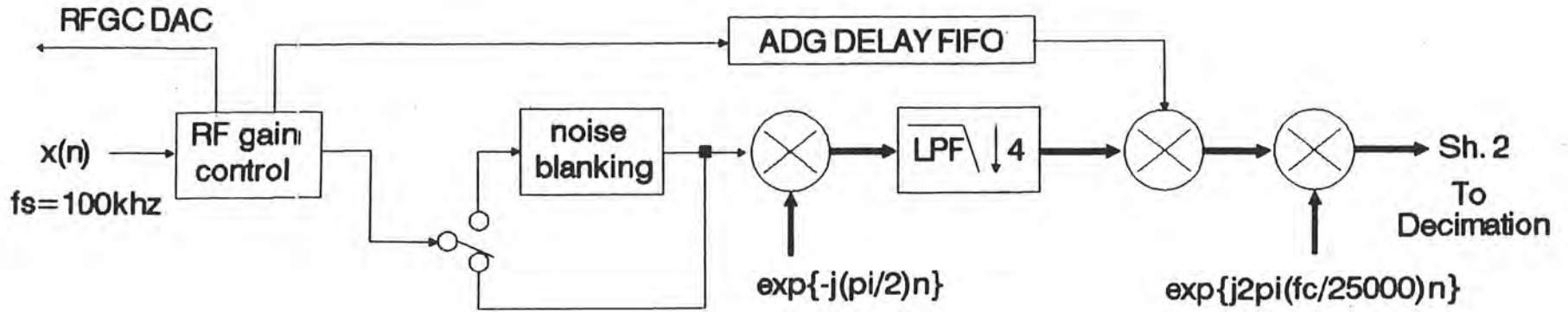


WJ-8711 DSP Block Diagram (Top Level) (Sh. 1 of 4)



f_s = sampling rate

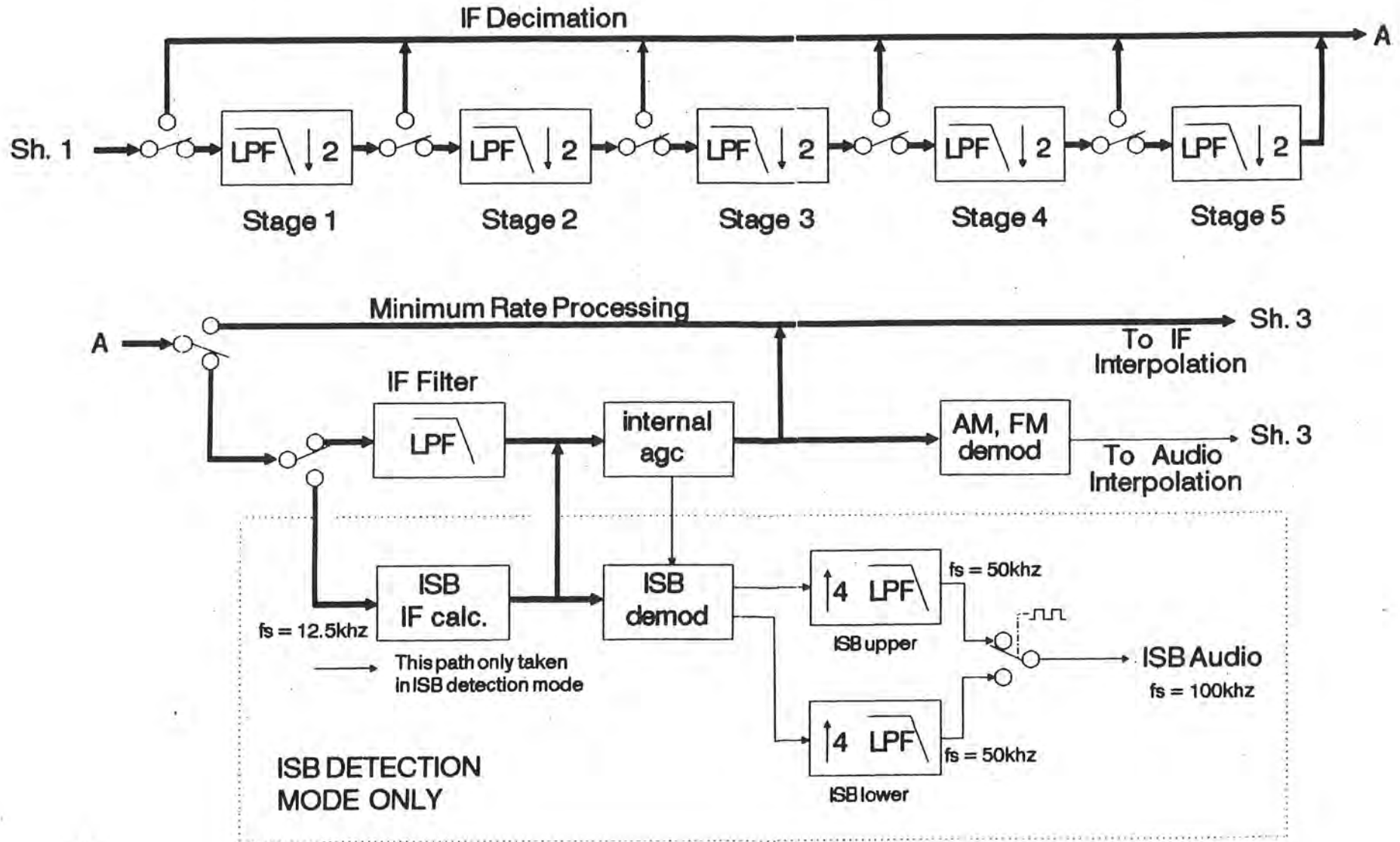
f_c = fine tune frequency

—————> Real Data

—————> Complex Data

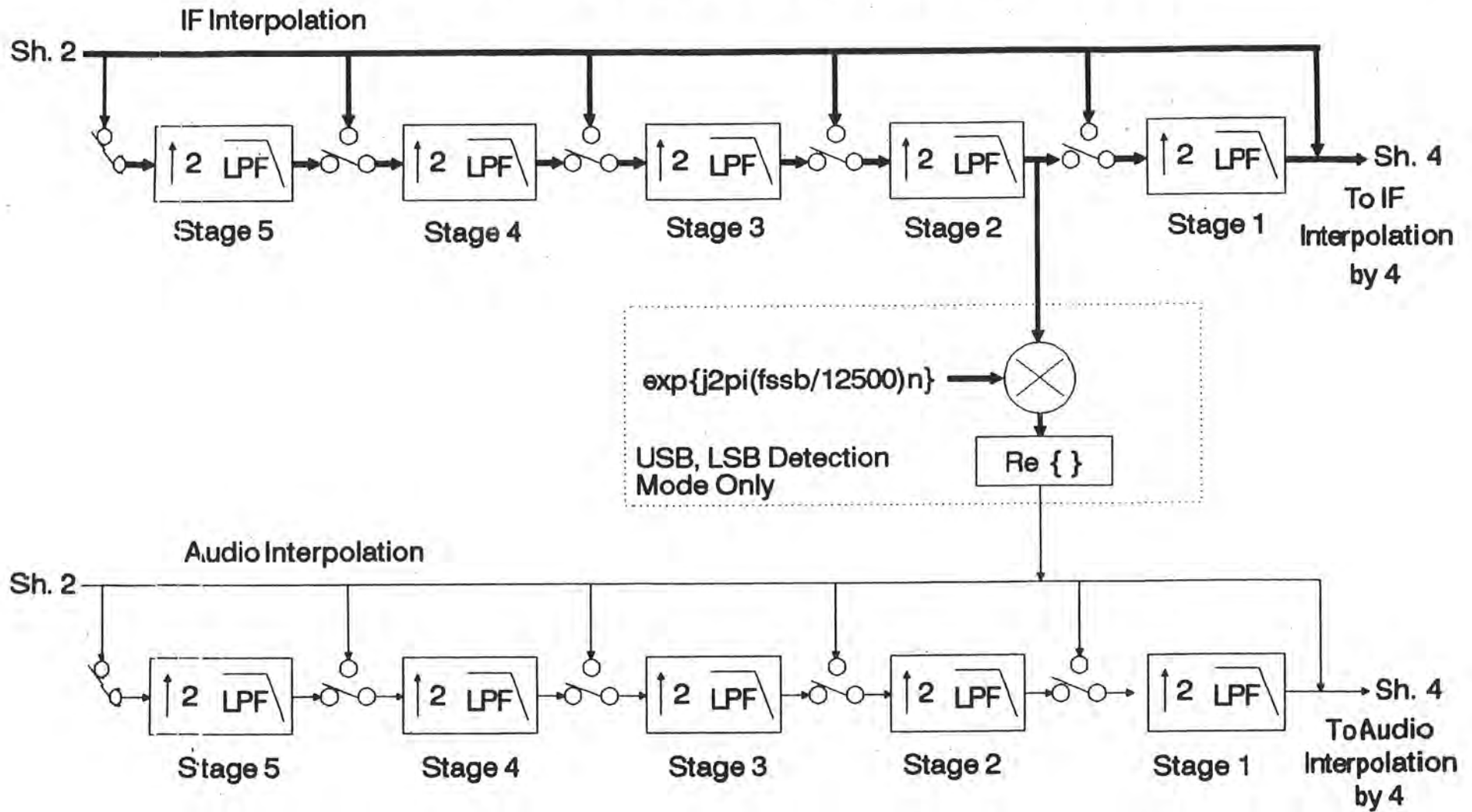
9/30/91
Fig. 1

WJ-8711 DSP Block Diagram (Top Level) (Sh. 2 of 4)



9/30/91
Fig. 1

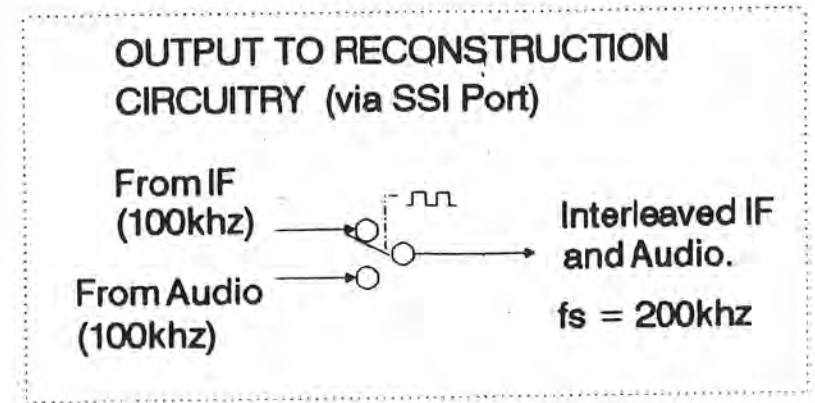
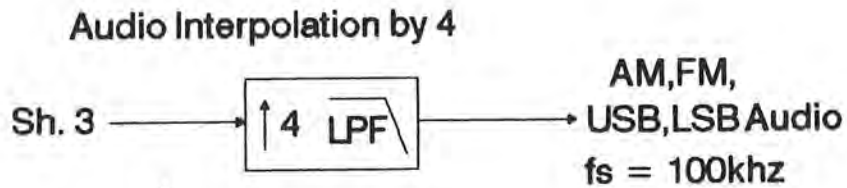
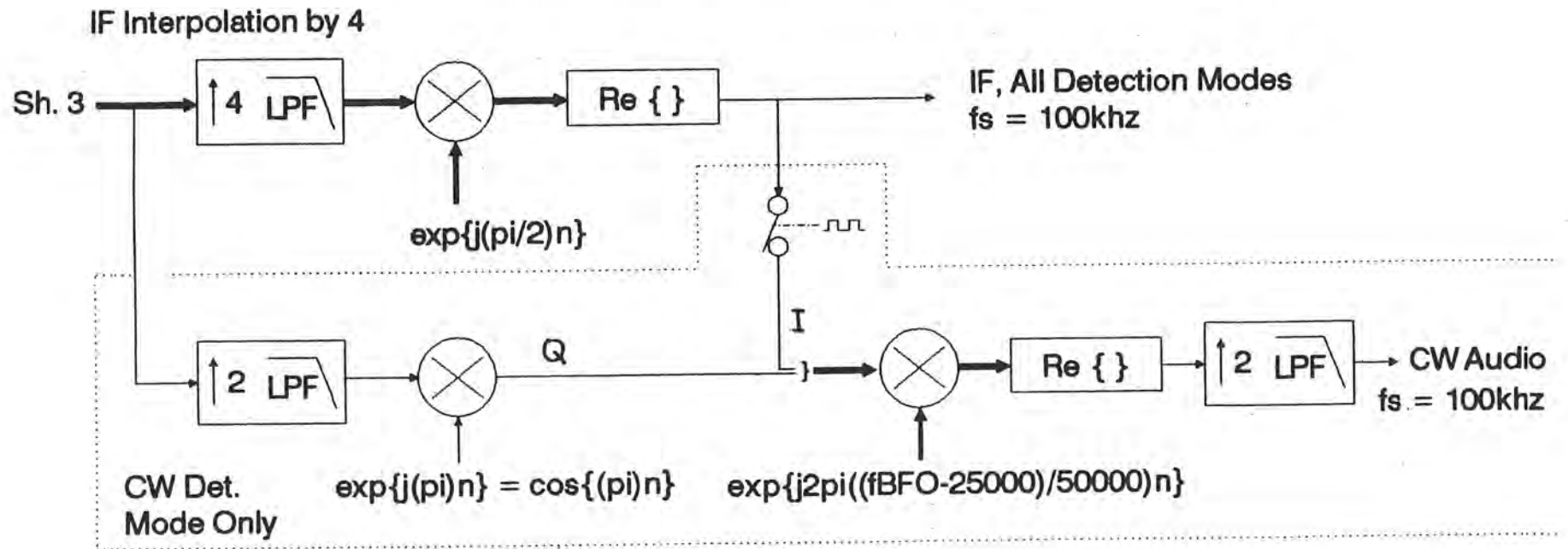
WJ-8711 DSP Block Diagram (Top Level) (Sh. 3 of 4)



9/30/91

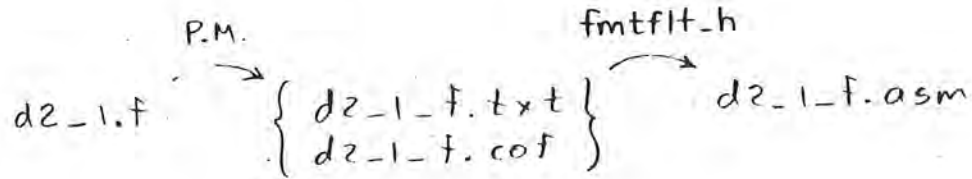
Fig. 1

WJ- 8711 DSP Block Diagram (Top Level) (Sh. 4 of 4)



9/30/91
Fig. 1

Decimation/Interpolation by 2



Decimation by 4

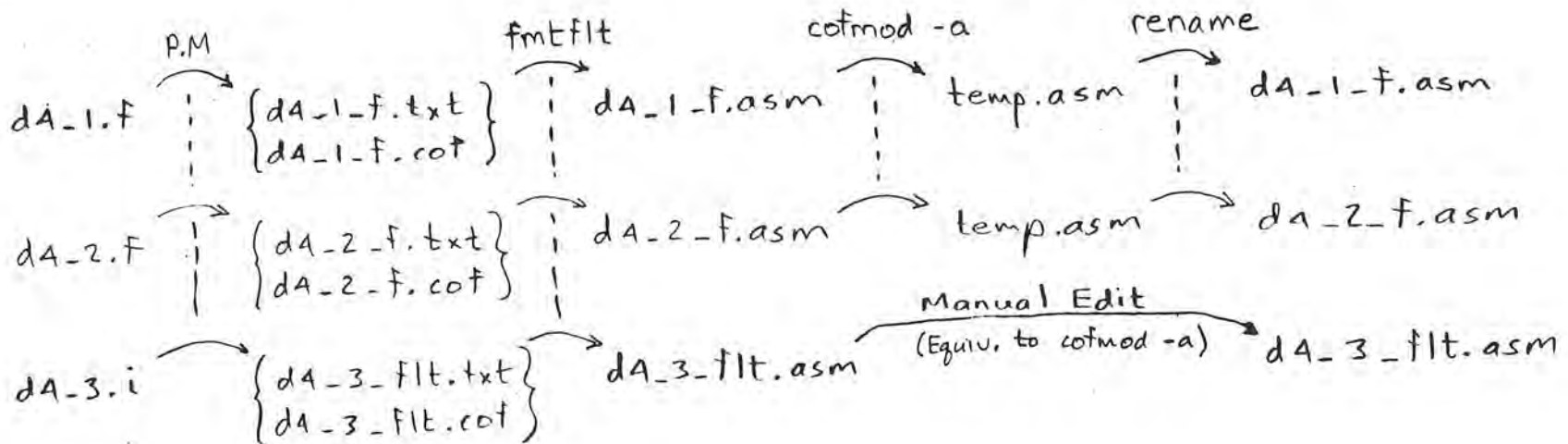


Fig. 16
1-f4

Interpolation by 4 (IF)

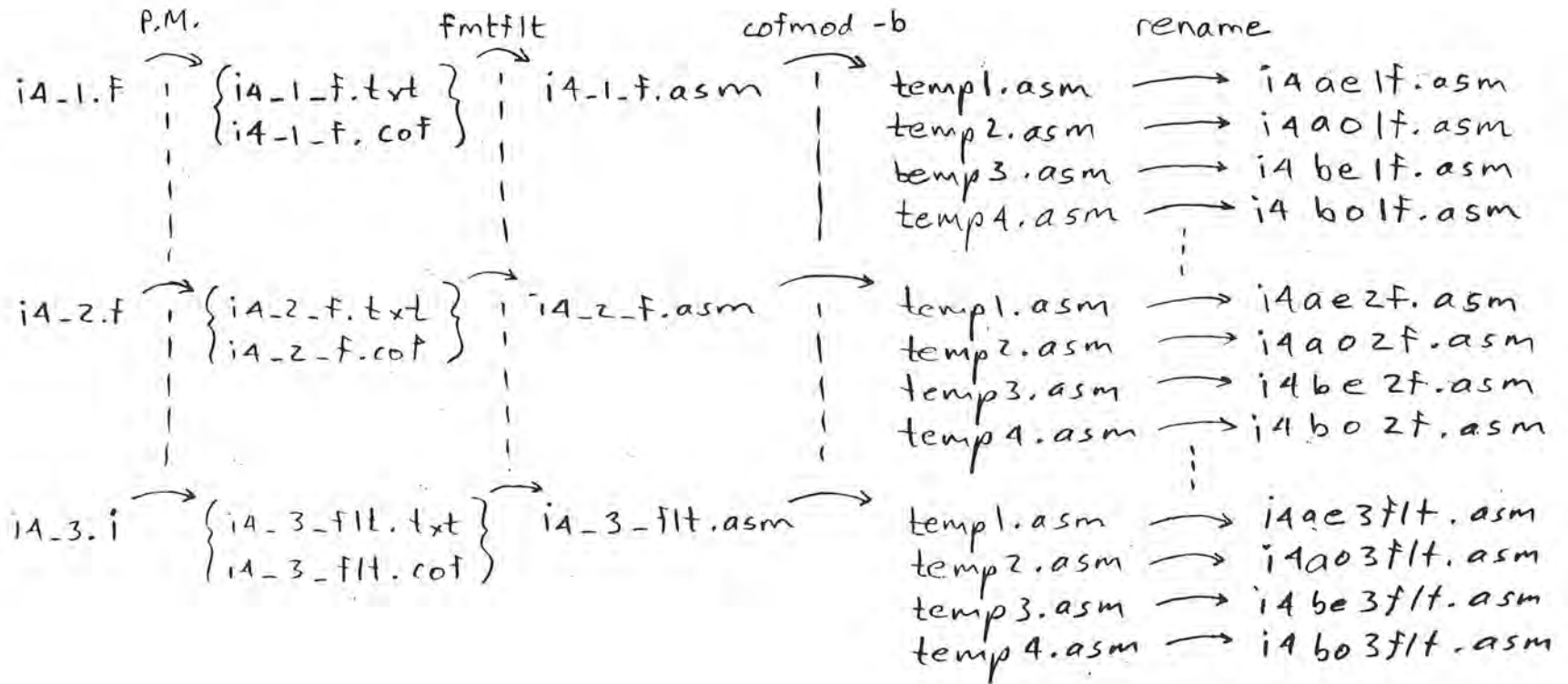
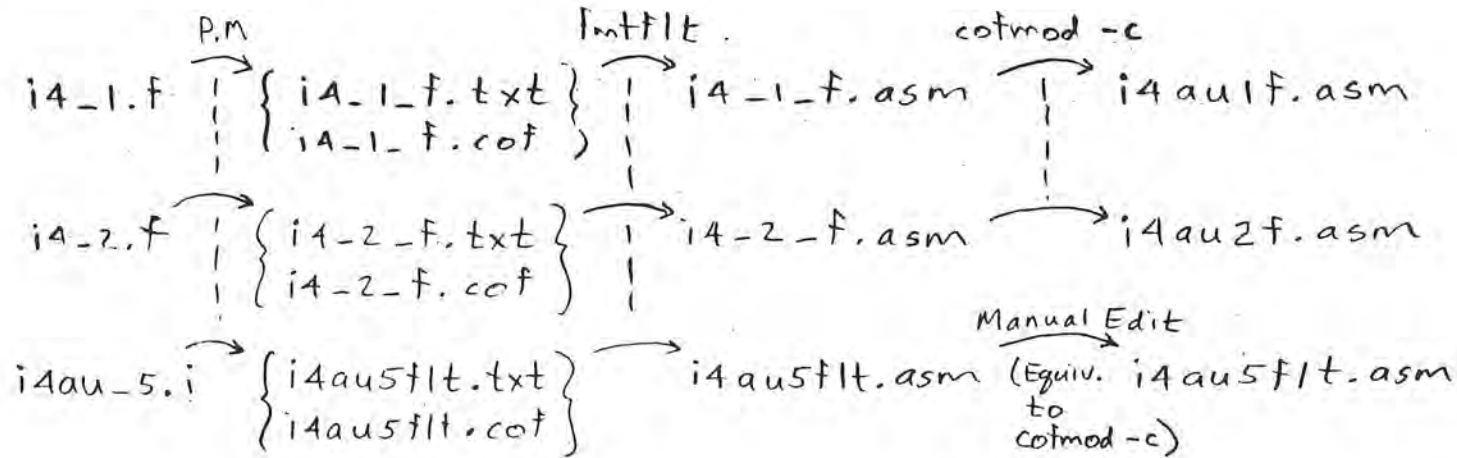


Fig. 16
2 of 4

Interpolation by 4 (Audio)



IF filters

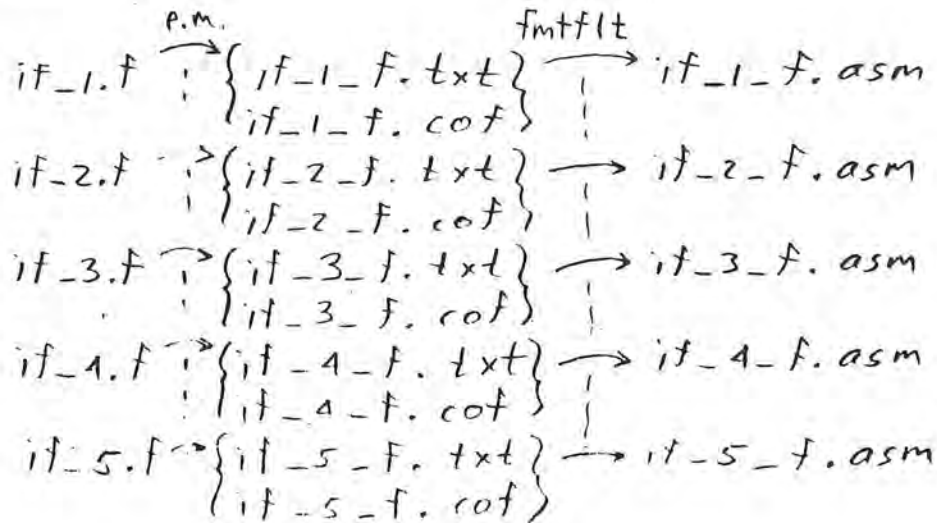
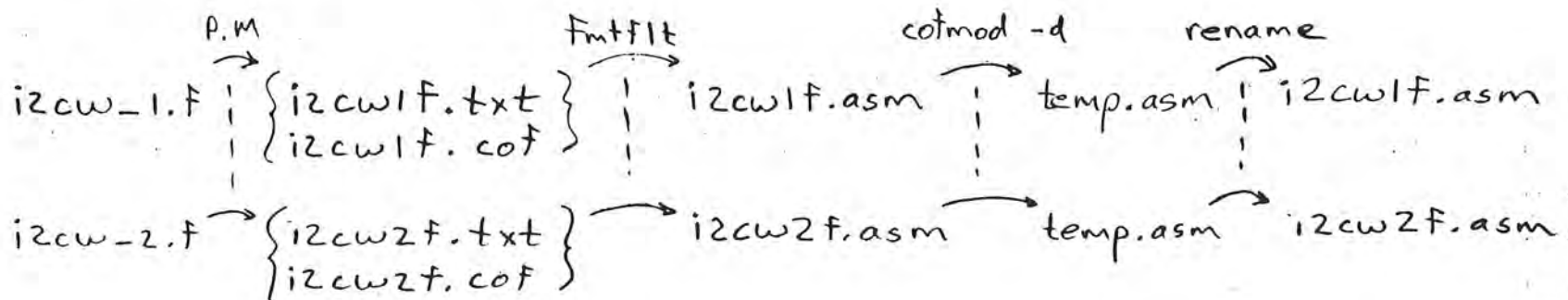


Fig. 16
3 of 4

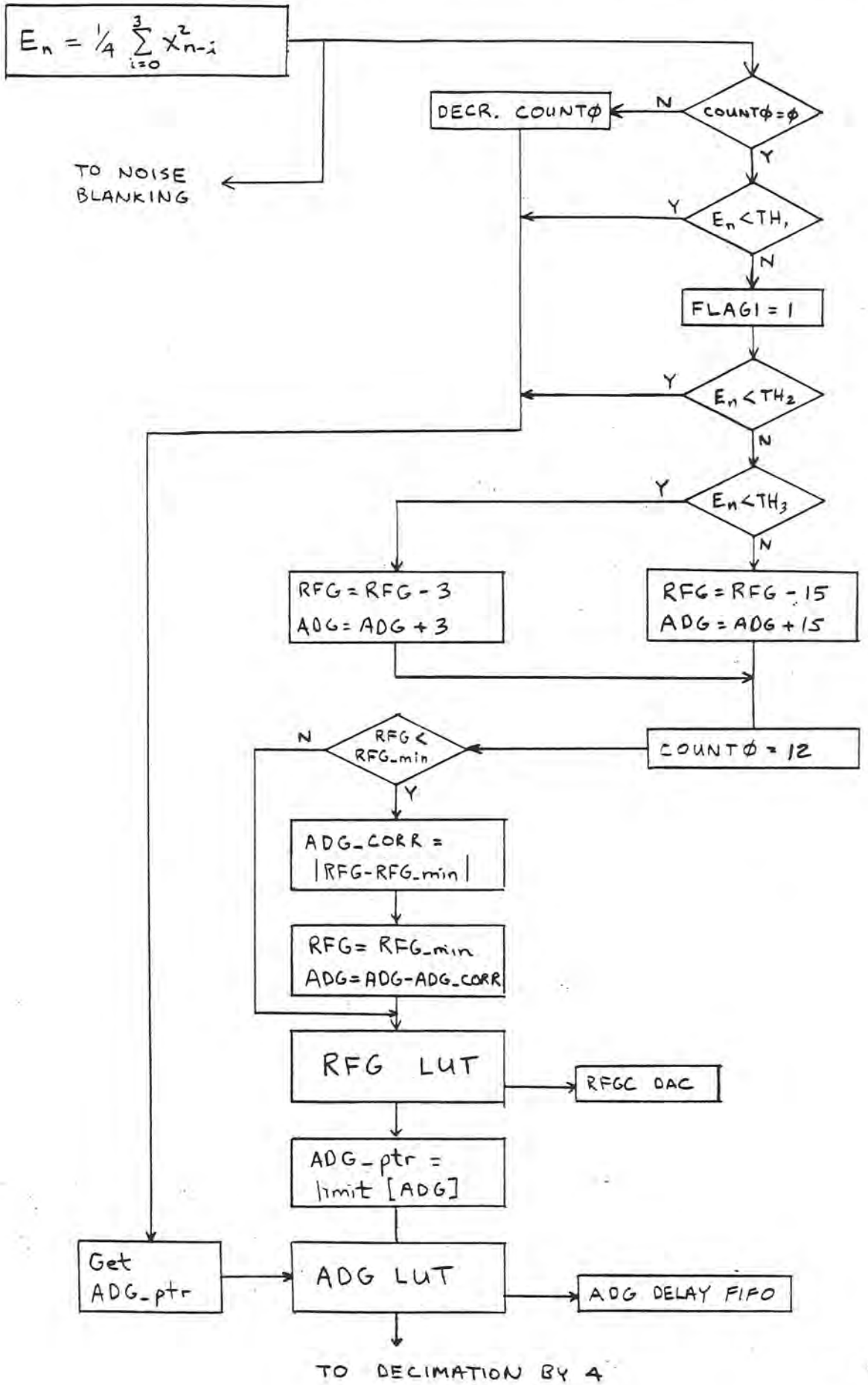
CW Audio Interpolation by 2

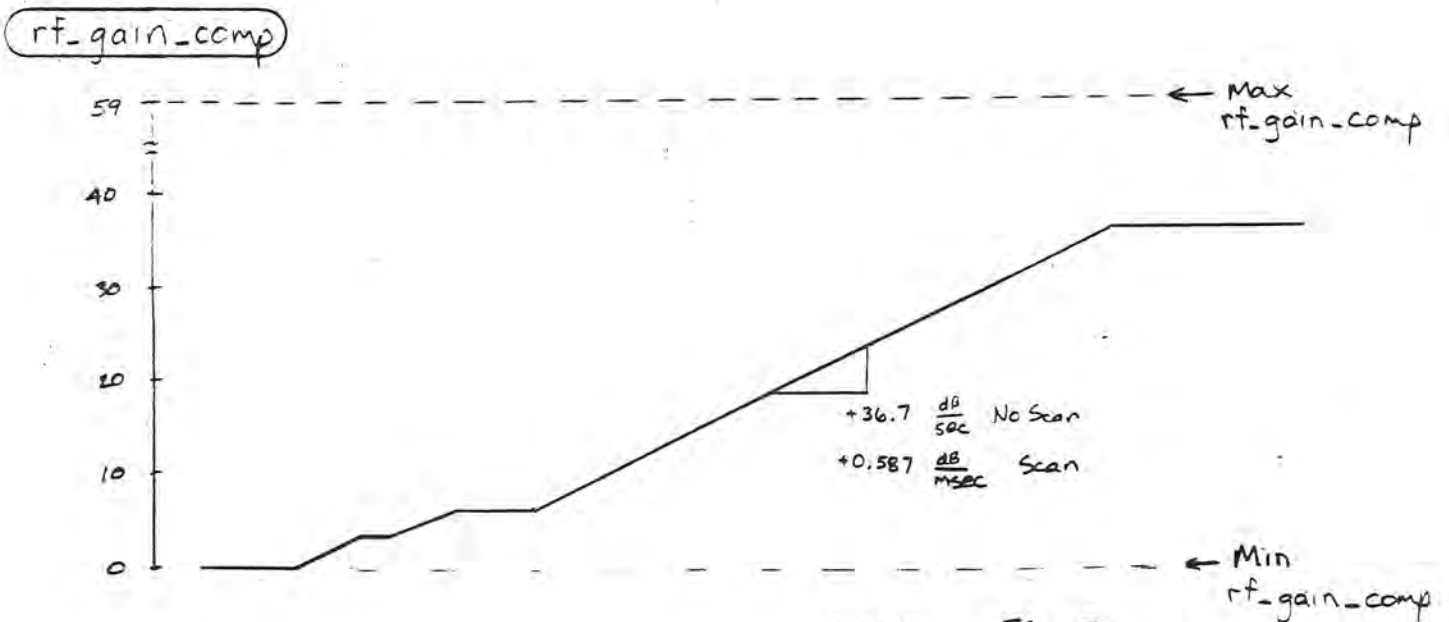
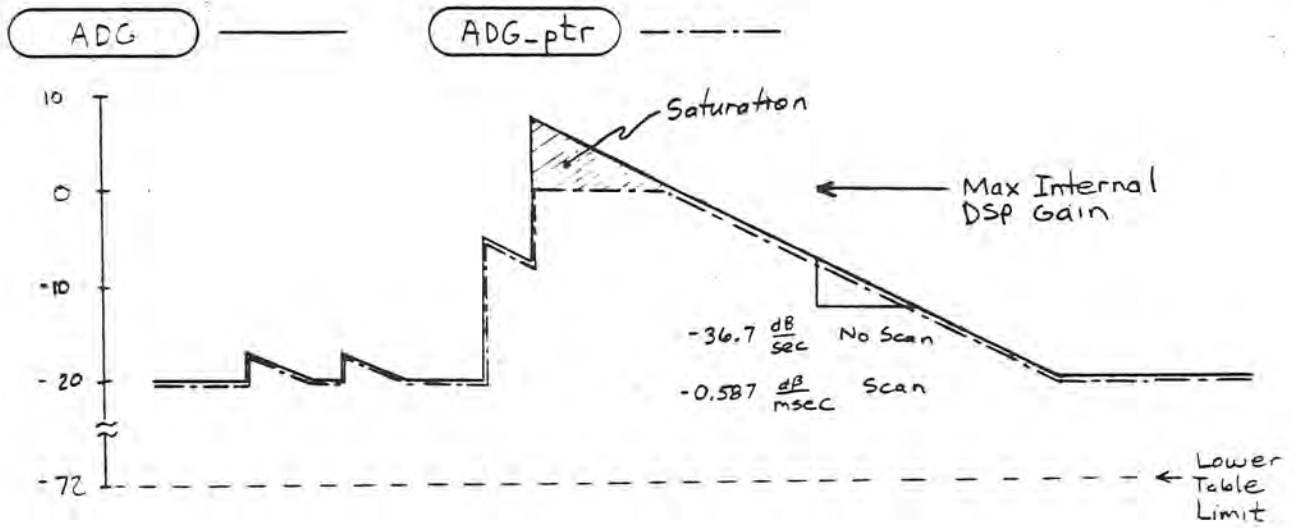
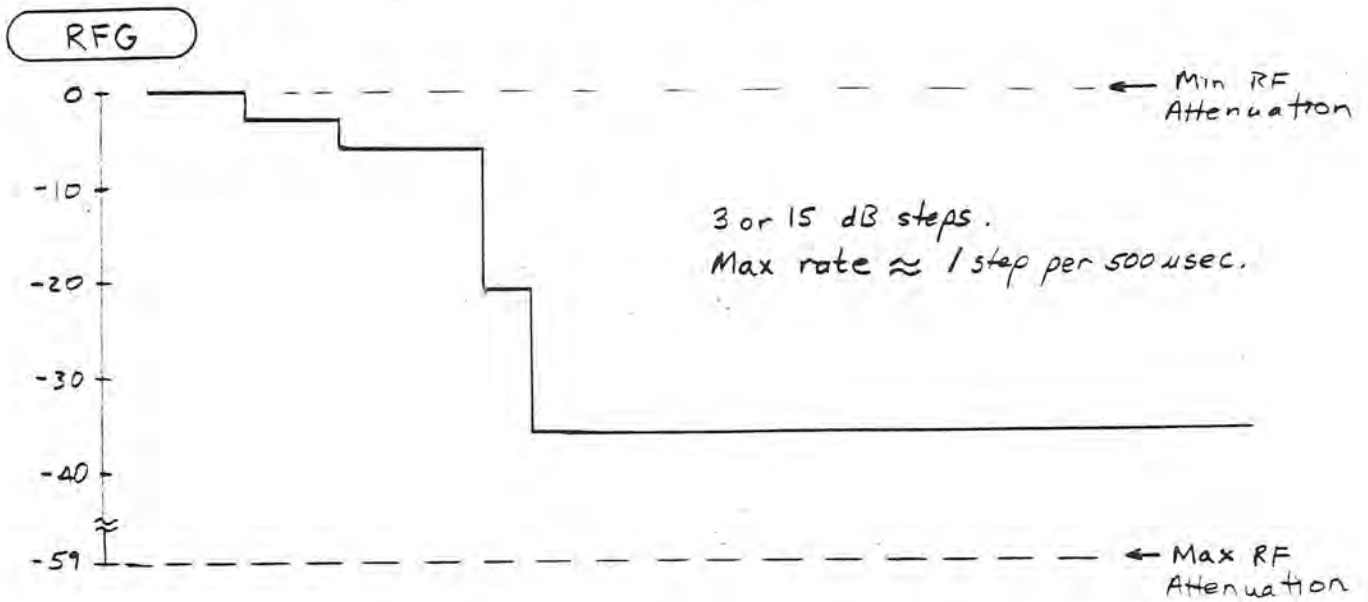


Set RF Gain Control per Scan Mode

Check Increase RF Gain Is Required

"Ramp" ADG toward nominal value



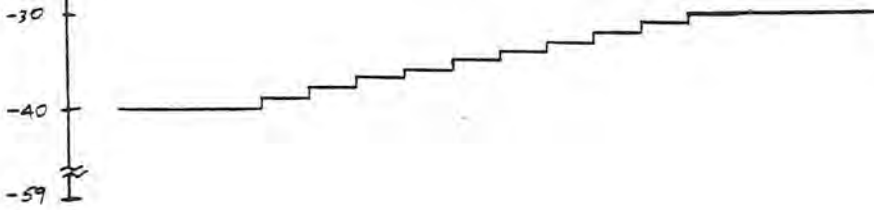


9/24/91 Fig. 5

RFG

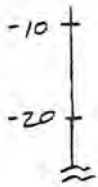


1 dB steps.
max rate: 1 step per 164 msec. Scan off.
1 step per 2.56 msec. Scan on.



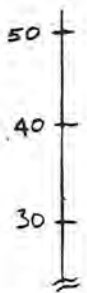
ADG = ADG_ptr

Since saturation doesn't occur in this example.



Scan off

rf_gain_comp



Scan off

Gain Control LUTs

Relative Address

$\$7F = 127$

$\$7E = 126$

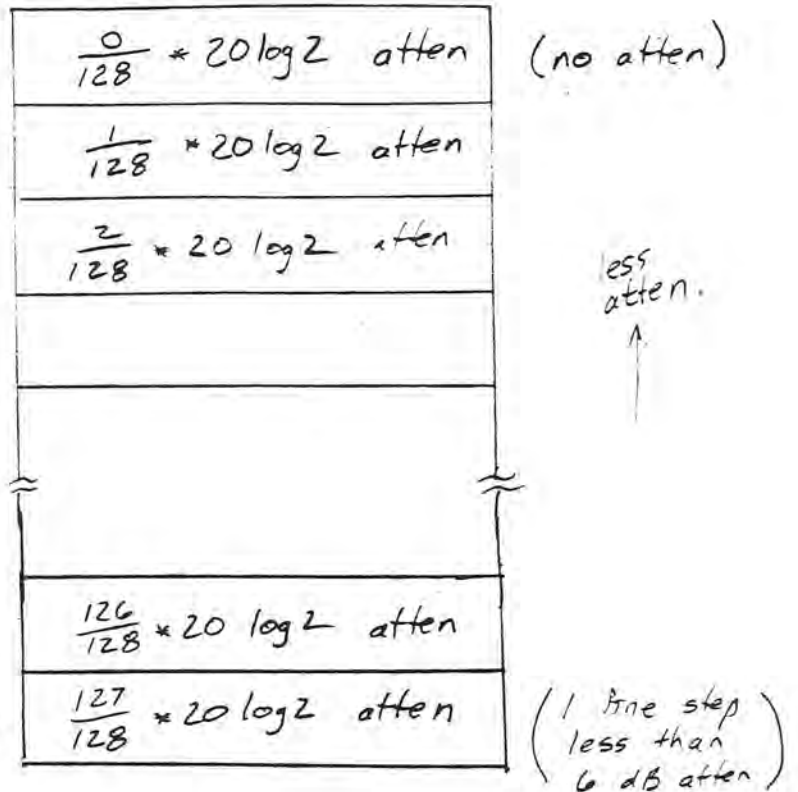
Each step is \rightarrow

$\frac{20 \log 2}{128}$ dB attenuation

Entries shown here are in dBs. The actual table has the linear value ($x \leq .9$)

$\$0 = 0$

FINE



COARSE

$\$1F = 31$

Transforms smallest possible value of $\$000001$ to $\$400000$. Any more gain would result in overflow:

$\$1 = 1$

$\$0 = 0$

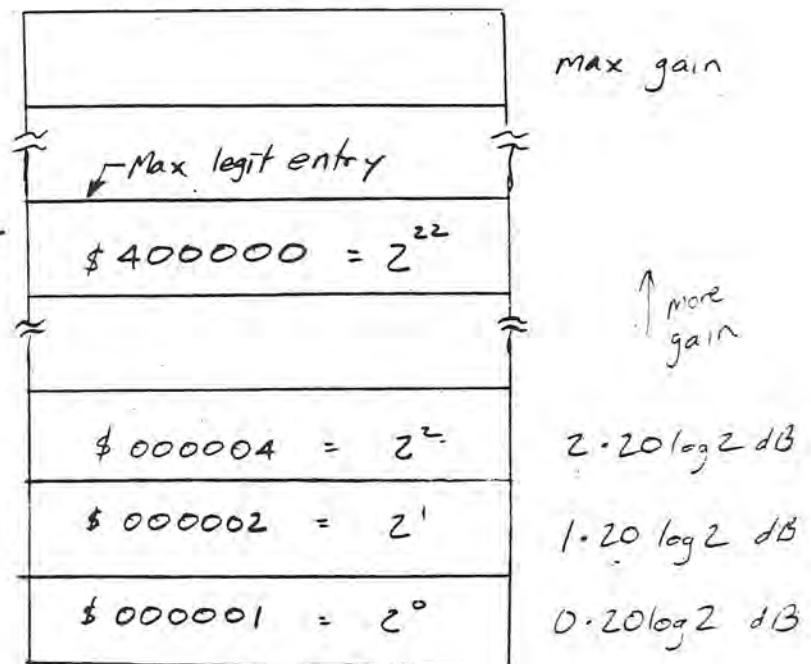
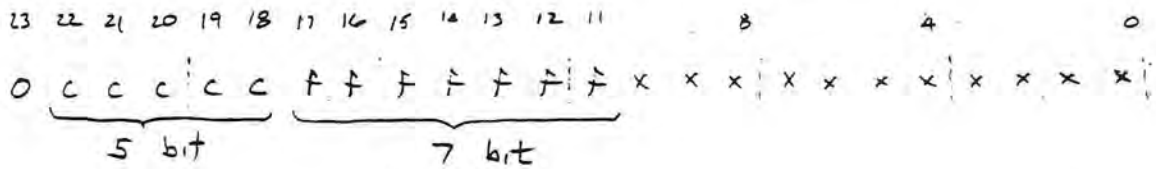


Fig. 11
10+2

Address Generation for LUT



Net gain = 5 bit coarse address * 20 log 2

minus $\frac{[127 - 7\text{bit fine address}]}{128} * 20 \log 2$ dB

Example: Address = $0 \underbrace{10110000}_{5\text{bit}} \underbrace{1011}_{7\text{bit}} x \dots$

Gain = $22 * 20 \log 2 - \frac{(127 - 11)}{128} * 20 \log 2$

Gain = 126.997 dB

Manual Gain

Save =
Manual Gain
approach.

This equation relates the gain produced from the two lookup tables to the value required to "feed" the LUT address generation code.

$$\text{Most significant bits} = \lfloor \text{SR} \left[\left(\frac{\text{Gain}}{128} \right) + 127 \right] \rfloor \leftarrow \text{Exact}$$

$$\text{Top 3 Hex digits} \approx \left[\left(\frac{\text{Gain}}{.047} \right) + 127 \right] / 2$$

Min Gain = -41.4 → ...FF D0F

$$\begin{array}{l} 111010000 \\ 1110100001111 = \$E87800 \end{array}$$

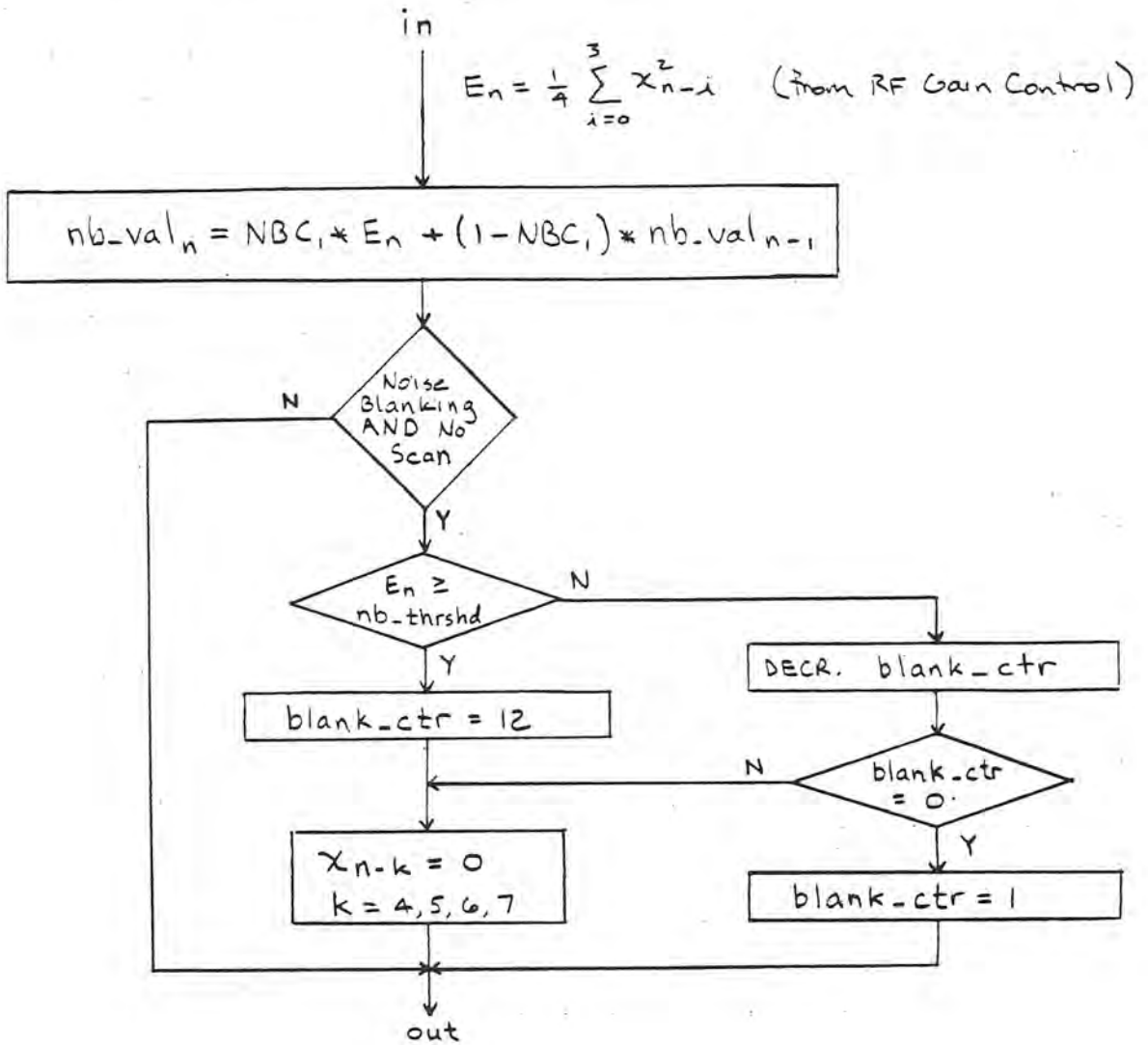
Max Gain = 96.0

Top 3 Hex digits ≈ 43D → 430000

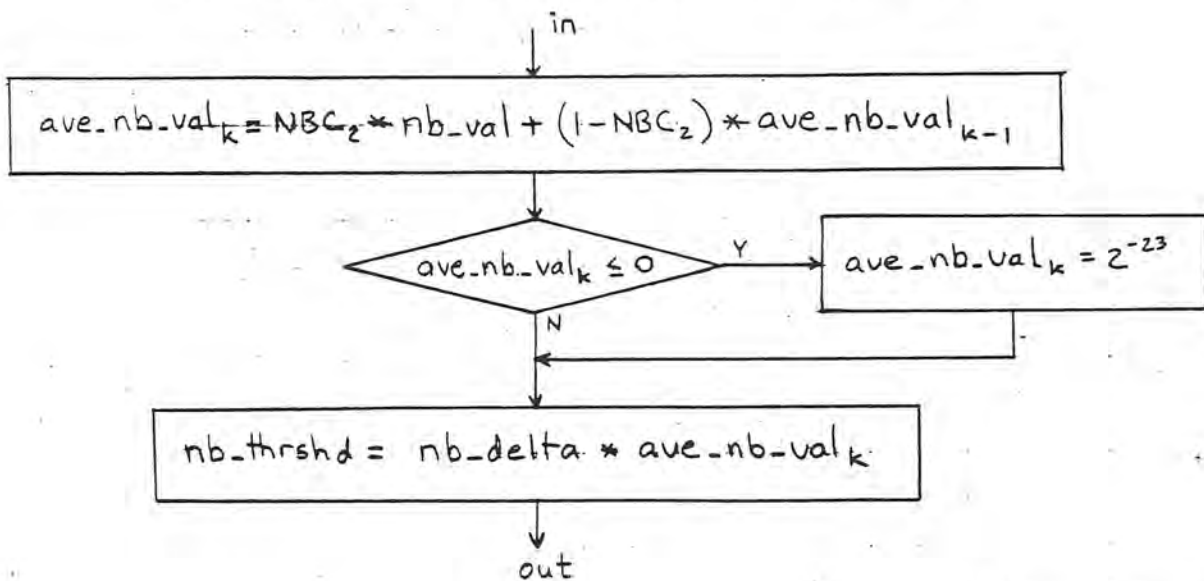
Table	Min Gain →	\$E87800 + 0 * 23 * (\$800)	
		\$E87800 + 1 * 23 * (\$800)	
		\$E87800 + 2 * 23 * (\$800)	
			Step size
		\$E87800 + 127 * 23 * (\$800)	

NORM 30A
ATTEN 40Z

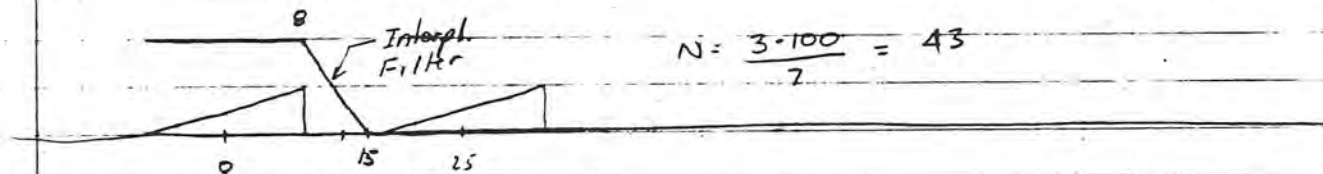
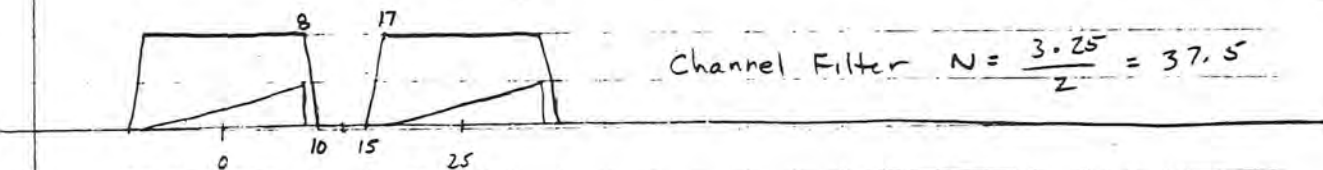
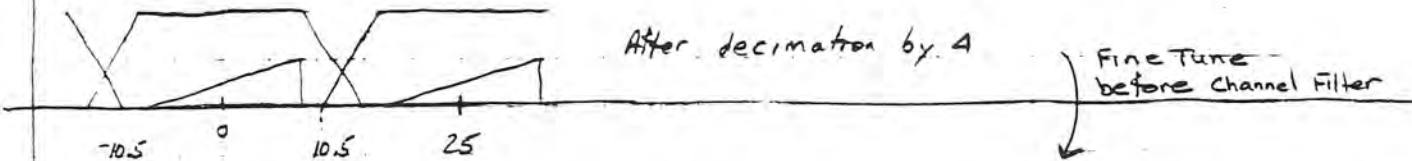
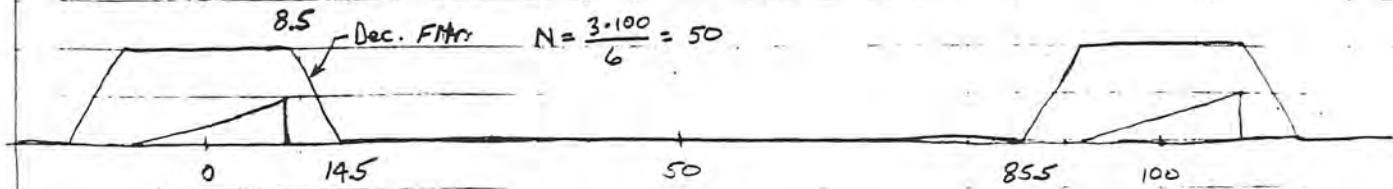
Fig. 12



P/O IRQB INTERRUPT SERVICE ROUTINE



Computations - Approach 2 (Dec. by 4)



Decimation $\rightarrow \frac{50}{4} = 12.5$

Ch. Filter $\rightarrow \frac{75}{4} = 18.75$

Interpolation $\rightarrow \frac{43}{4} = 10.75$

42

Intpl Filter could be the same as dec. filter to save storage. cost would be $\frac{7}{4}$ Instr.

Note: These filters were tweaked a little so the frequencies shown are not exact. See filter files for exact values.

However, filters are stored differently to minimize overhead.

Fig. 8

Decimation by 4 with $f_s/4$ Translation Down

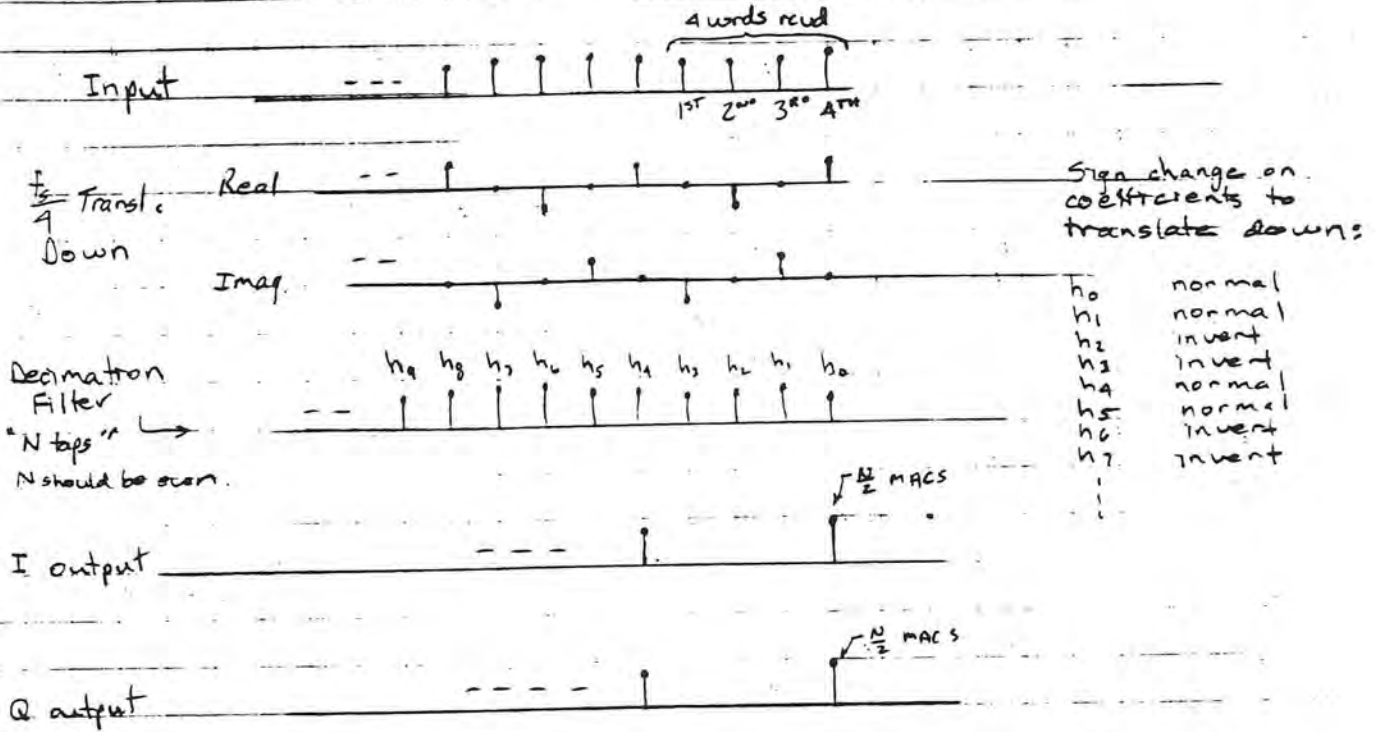
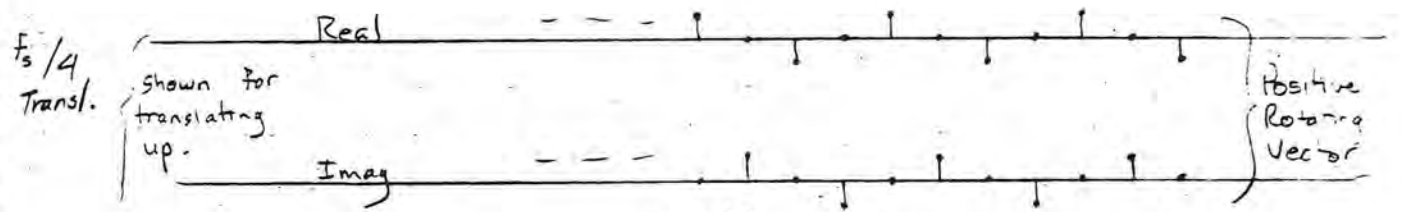
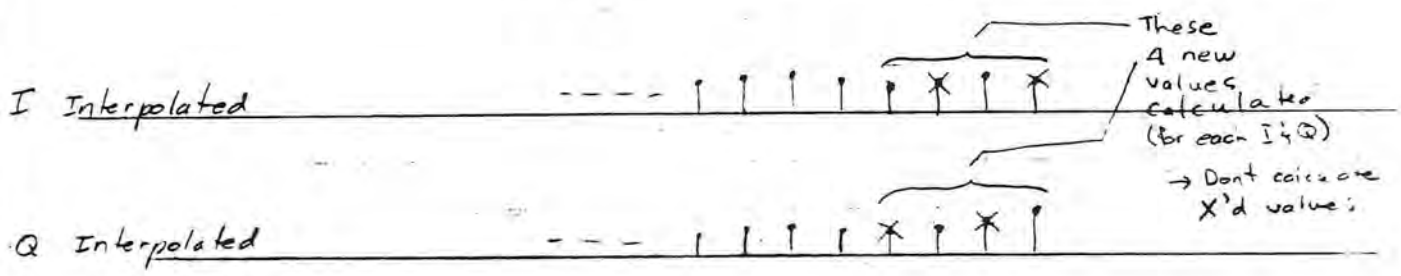
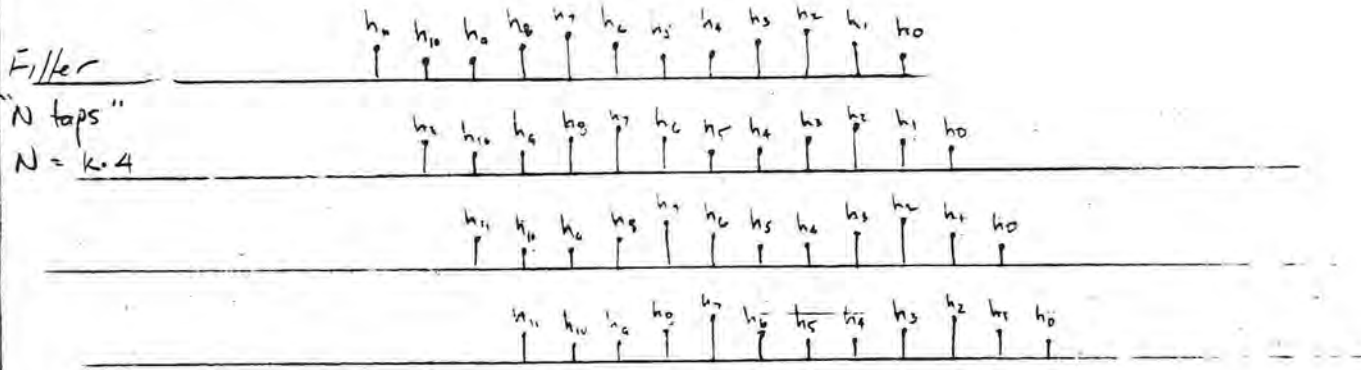
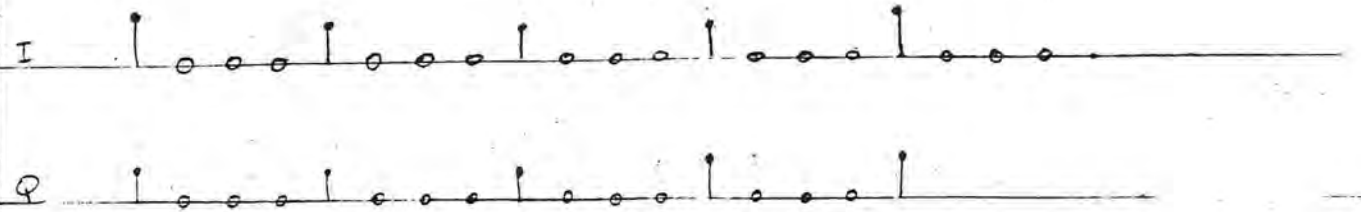


Fig. 9

Interpolation by 4 w/ $\frac{f_s}{4}$ Translation Up



Interpolated Data $\xrightarrow{\frac{f_s}{4} \text{ transl.}}$

$$\text{Output} = \text{Real} \left\{ (I + Qj)(\text{Real} + \text{Imag}j) \right\}$$

NOTE CHANGE

$$= I \cdot \text{Real} - Q \cdot \text{Imag}$$

Sign change to accomplish $\frac{f_s}{4}$ up translation; taking real part

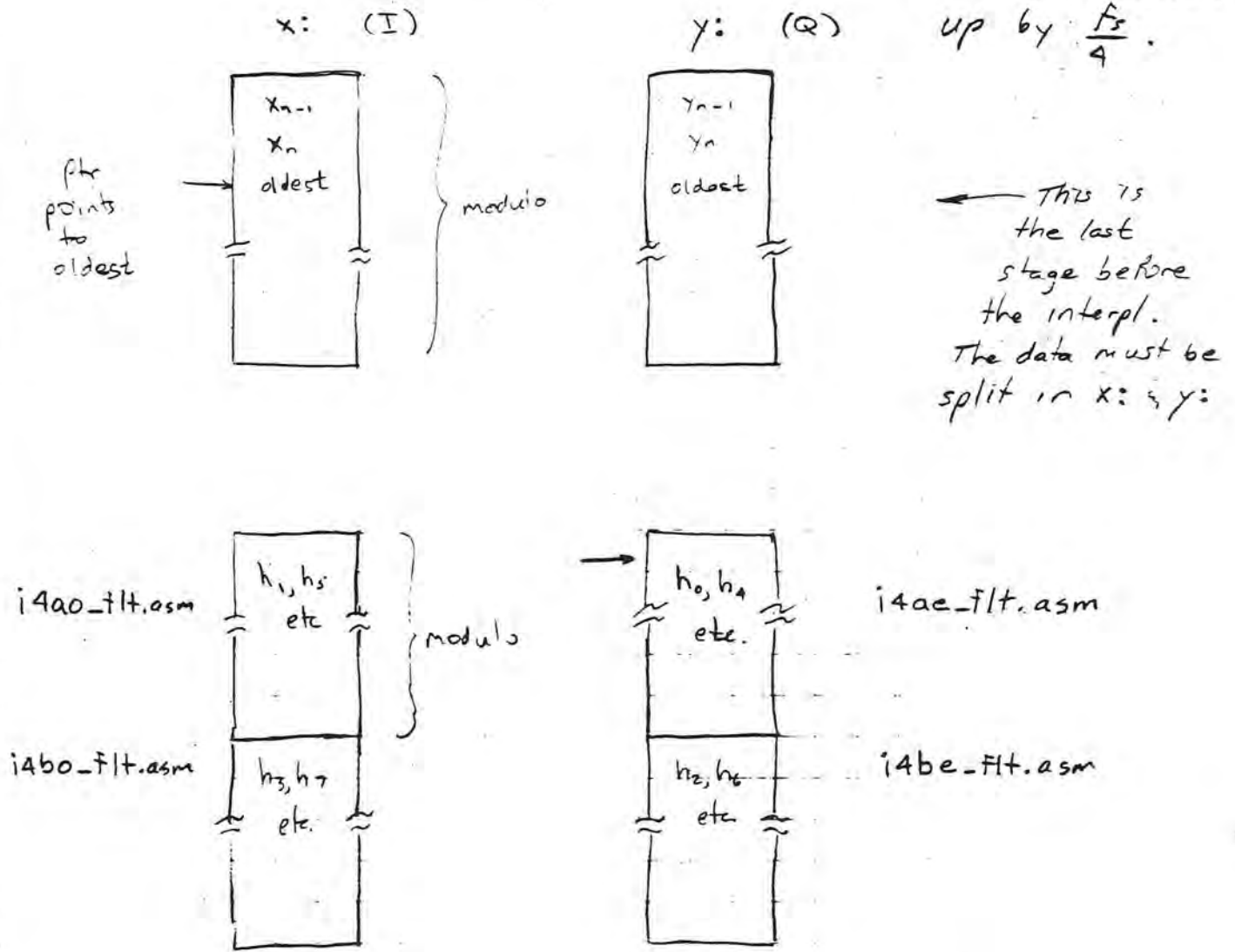
^ Invert the Imag. to accomplish this negative

- | | | |
|----------------|--------|---|
| h ₀ | normal | } |
| h ₁ | invert | |
| h ₂ | invert | |
| h ₃ | normal | |
| h ₄ | normal | |
| h ₅ | invert | |
| h ₆ | invert | |
| h ₇ | normal | |

CHANGED TO for upright IF spectrum.
 (required $\frac{f_s}{4}$ translation DOWN versus original UP)
 ↳ UP would have worked except analog IF was inverted spectrum

Fig 10
1of2

Buffer & Filter Structure for Interpolation with Translation up by $\frac{f_s}{4}$.



NOTE: This still requires an address reg. update after calculating two values.

If I & Q were interleaved in x: and coefficients were in y:, the extra overhead would be:

	Instr
load n reg. with #2.	1
update coeff ptr, data ptr.	3

Fig 10
(cont.)
2 of 2

Sig Strength Reporting

$$\text{Intgn_gn} = -29 - X \text{ dBm}$$

This is the required integration gain to bring an X dBm signal up to the set point (Normal RF input)

$$\text{Intgn_gn} = -29 - (-135) = 106$$

$$\text{Intgn_gn} = -29 - (+20) = -49$$

Signal Level	Intgn Gain (-15 dB Atten)	Intgn Gain (Normal)	Intgn Gain (+10 dB)
-135	106 + 15	106	106 - 10
-134	105 + 15	105	105 - 10
-133	104 + 15	104	104 - 10
⋮		⋮	
-30		1	
-29		0	
-28		-1	
-1		-28	
0		-29	
1		-30	
2		-31	
⋮			
20		-49	

↑
NOTE: Since the integrator is 15 dB higher, 15 has to be subtracted to get the real representation of the signal level

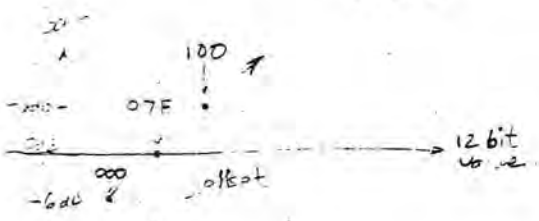
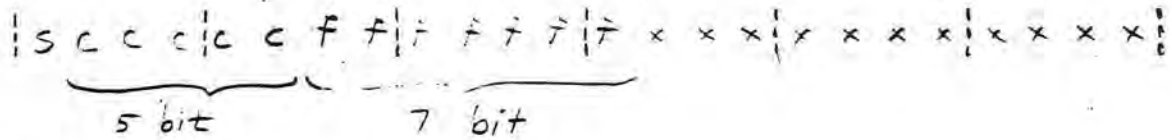
↑
NOTE: same thing here. Add 10 dB to the integr output.

This value exists in the code in IRQB

Fig. 15
10+3

Sig Strength Reporting

The output of the integrator has the following format.



This bit represents $\frac{20 \log 2}{4} = 1.5051 \text{ dB}$

See next page

The integrator (for Normal RF input) must range from +106 dB to -49 dB. This requires 7 bits of magnitude plus the sign bit.
 Really (1.5051 - 5.97) dB due to offset. See next page.

Algorithm: (Start w/ the intgn value that already is ^{RF input accounted for})

① Mpy the intgn gain value by 1.5051 so the indicated bit above represents 1.0 dB.

16 bit shift → ② Mpy the result by a shift constant which will shift the result so the magnitude occupies bits [6:0] (A 16-bit shift right)

$(1.5051)(0000080) = 000022966$ { Combine ① & ② } Do an mpy

COMPOSITE MULTIPLIER for ① & ②

③ The max Intgn-gain for normal RF input is ~~106~~ for -135 dBm signals. This will give a 0 value for the Host.

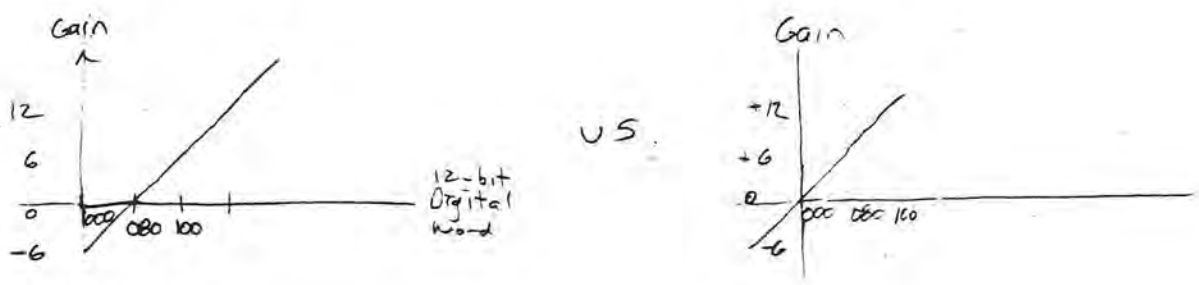
Negate the result of ① & ② and add ~~106~~
 Limit the range from 0 to 155
 Fig. 15 2 of 3
 See next page.

12 bit code		dB
coarse	fine	
0 0 0 0 0	0 0 0 0 0 0 0	-5.97 dB
0 0 0 0 0	0 0 0 0 0 0 1	-5.93 dB
0 0 0 0 0	0 0 0 0 0 1 0	-5.88 dB
<hr/>		
0 0 0 0 0	1 1 1 1 1 1 1	0 dB
<hr/>		
0 0 0 0 1	0 0 0 0 0 0 0	6.02 - 5.97
0 0 0 0 1	0 0 0 0 0 0 1	6.02 - 5.93
0 0 0 0 1	0 0 0 0 0 1 0	6.02 - 5.88
<hr/>		
0 0 0 0 1	1 1 1 1 1 1 1	6.02 dB

} 128 steps of
 $20 \log_2 2/128$

← 7 bits representing magnitude of the output of the integrator.

This illustrates the fact that the gain vs 12-bit digital word has an offset of about 6 dB



A
This can be compensated for by adding 112 in the algorithm vs 106.

RESULTS: I checked this out and it appeared to be working (to within about a dB) over the range -130 to +10. I didn't go beyond those limits.

Fig. 15
30+3

The desirable format for running the program is

```
prog1 <arg1> <arg2>
```

with <arg1>.asm being a user specified source file and <arg2>.asm being a user specified dest file.

The same is true for the 3RD & 4TH cases.

The 2ND case where there are 4 output files could just append 1, 2, 3, 4 to <arg2> so the 4 output files would be

<arg2>1.asm	h0, h4...
<arg2>2.asm	h1, h5...
<arg2>3.asm	h2, h6...
<arg2>4.asm	h3, h7...

The four cases on the previous sheet are options -a, -b, -c, -d respectively;

The program is cotmod.c.

EPROM organization.

→ The address in the .LOD file is 1/3 the EPROM address where the data will be stored.

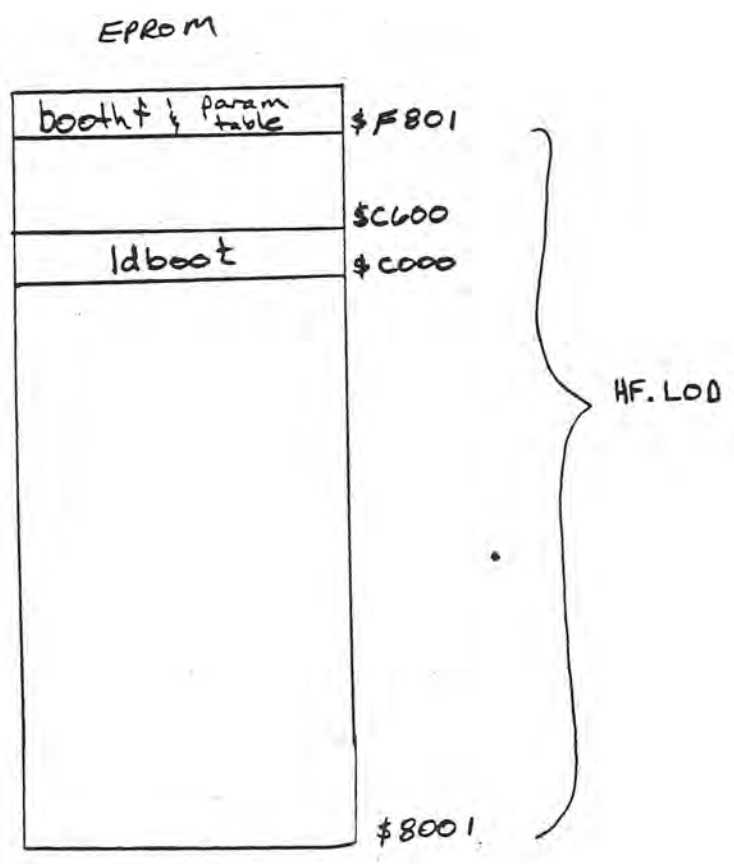


Fig. 18
2 of 2